Asymptotic Calculation of the Biot's Waves in Porous

Layered Fluid-Saturated media

A Thesis

Presented to

the Faculty of the Department of Earth and Atmospheric Sciences

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In Partial Fulfillment

of the Requirements for the Degree

Master of Science

By

Yangjun (Kevin) Liu

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ABSTRACT

This work uses the asymptotic analysis of Biot's poroelasticity theory (Goloshubin et al., 2008) to model the seismic response from porous permeable fluid-saturated reservoir. The Thomson-Haskell propagator matrix method is utilized for solving the Fast P wave and Biot's Slow wave propagation through the multi-layered media. We derived the propagator matrix for the normal incidence mode conversion between P wave and Biot's Slow wave and programmed it into a Fortran code. This code calculates the reflectivity and transmitivity series of a fluid zone and obtains the influence of the Slow P wave on the seismic signal.

Our results show that for a reservoir with homogeneous fluid saturation, Slow P wave effect is negligible. If the rock is inhomogeneous in either fluid saturation or permeability, a significant Slow P wave effect can be observed. The Slow P wave effect is very sensitive to frequency and has a strong similarity with the observed low frequency shadows. It is highly possible that the low frequency shadows frequently observed under gas reservoirs are induced by the fluid flow in the reservoir and the propagation of the Slow P wave.

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CHAPTER 1: Introduction

Biot's poroelasticity theory (1956a, b) predicts movements of the pore fluid relative to the skeleton as seismic waves propagate through the reservoir. This phenomenon opens an opportunity for investigation of fluid properties of the hydrocarbon-saturated reservoirs from seismic amplitude. According to Biot, a compressional P wave in a fluid-saturated porous medium is a superposition of slow and fast waves. These two waves are always coupled and coexist with each other, so that in a fluid-saturated porous permeable rock, three types of waves exist: classical P wave, Shear wave, and Biot's Slow wave, as shown in Figure 1. The left figure shows wave propagation at a pure elastic boundary, where only P wave and shear wave exist, the right figure shows wave propagation at a porous permeable elastic boundary, where P wave, Shear wave and Biot's Slow wave would exist.

One application of Biot's theory is the study of Dutta & Ode (1983). They used Biot's model to calculate the seismic reflections from a gas-water boundary in a porous sand reservoir. Velocity, attenuation, and angular-dependent reflection and transmission at both gas and water layers for the frequency range $0 \sim 10^5$ Hz were obtained. They concluded that in a fluid-saturated porous rock, loss of seismic energy is mainly due to the mode conversion to Biot's Slow wave and they are proportional to $f^{1/2}$, where f is the frequency. There is about 2.5 percent of energy loss due to mode conversion to Biot's Slow wave at 100 Hz. Thus, They suggested that in fluid saturated rock, effects due to Slow wave should be taken into account.

Dutta & Ode (1979a, b) and Dutta & Seriff (1979) studied the attenuation of seismic wave in a fluid-saturated porous rock with partial gas saturation (White, 1975) using Biot's theory and modified White's model, respectively. Both theories conclude in good agreement with each other. They also pointed out that the energy dissipation for their model is mainly due to the relative fluid flow from Biot's Slow wave. Three different geometries of gas-filled zones are analyzed and compared in this study. They are: sphere model, shell model, and layer model. While in terms of magnitude of the attenuation, all three models behave similarly.



Figure 1. Reflection and refraction of a wave from elastic boundary and from a porous permeable elastic boundary.

Carcione et al. (2003) utilized a poroelastic modeling algorithm to compute wave propagation in White's spherical gas pockets model. Their results also confirm that the conversion of fast P wave into Biot's Slow wave is the main mechanism of attenuation for a partial gas saturated, brine-filled porous rock.

Our work presented here utilizes a propagator matrix method to calculated fullwave reflectivity series from a fluid-saturated porous permeable rock that composed of layered media, reflection and transmission coefficients through medium boundary are provided by asymptotic solutions of Biot's theory (Silin & Goloshubin, 2008). In this case, only normal incident scenarios are calculated, given the full solution of asymptotic analysis of Biot at normal incidence. Our result shows that Slow wave effects may appear in a seismic section as some real P wave reflectors. Its relative amplitude strongly depends on frequency and fluid type. When partial gas saturation exists in a fluid-saturated porous permeable rock, Slow wave effect is significantly enhanced. Agree with previous studies, conversion from P wave to Slow wave is the main mechanism of energy loss. Resonance due to recursive reflection of Slow waves among layers is possible, which would strongly enhance the seismic amplitude. This occurs only at very small sample rate such as 0.1 ms, since Slow wave effect can be resolved before all attenuated. If the sample rate are taken to be 1 ms \sim 4 ms, resonance due to Slow wave is less likely to occur. Slow wave in this study only refers to Biot's Slow wave, classical P wave is also called to Fast P wave.

CHAPTER 2: Asymptotic Calculation

2.1 Fast P wave as incident wave

Present work applies asymptotic formulas of Silin and Goloshubin (2008) to calculate reservoir models that constitute thin layers of gas and water layers. First, I study the seismic reflection from a single gas-water contact. In this situation, only the normal incident P wave is treated as the input wave, the output waves include both the reflected and transmitted fast and slow waves. They are denoted by R^{FF}, T^{FF}, R^{FS}, T^{FS}, and can be written in the asymptotic form as follows:

$$\begin{split} R^{FF} &= \frac{Z_{1}^{F} - Z_{2}^{F}}{Z_{1}^{F} - Z_{2}^{F}} + R_{1}^{FF} \frac{1+i}{\sqrt{2}} \sqrt{|\varepsilon|} + \dots \\ T^{FF} &= 1 + \frac{Z_{1}^{F} - Z_{2}^{F}}{Z_{1}^{F} + Z_{2}^{F}} + T_{1}^{FF} \frac{1+i}{\sqrt{2}} \sqrt{|\varepsilon|} + \dots \\ R^{FS} &= R_{1}^{FS} \frac{1+i}{\sqrt{2}} \sqrt{|\varepsilon|}; \text{ and } T^{FS} = T_{1}^{FS} \frac{1+i}{\sqrt{2}} \sqrt{|\varepsilon|}; \end{split}$$

where, Z_1 and Z_2 are the modified acoustic impedances of medium 1 and 2:

$$Z = \frac{M}{\nu_b} \sqrt{\frac{\gamma_\beta + (\gamma_M)^2}{\gamma_\beta}};$$

Here, $M = K + \frac{4}{3}\mu$ is the plane wave modulus from the dry rock bulk modulus K

and shear modulus μ , $\nu_b = \sqrt{\frac{M}{\rho_b}}$, (ρ_b is the bulk density) and γ_β , γ_M are given by:

$$\gamma_{\beta} = M \left(\beta_f \phi + \frac{1 - \phi}{K_{fg}} \right) \text{ and } \gamma_M = 1 - \frac{(1 - \phi)K}{K_{sg}}$$

where, $\beta_f = \frac{1}{K_f}$ is the fluid compressibility.

Also, first order refelction and transmission coefficients R_1^{FF} and T_1^{FF} have the forms:

$$R_1^{FF} = \frac{Z_2(T_1^{FS} - R_1^{FS})}{Z_1 + Z_2}$$
; and $T_1^{FF} = \frac{Z_1(R_1^{FS} - T_1^{FS})}{Z_1 + Z_2}$.

We assume i = 1 is the medium above the boundary, i = 2 is the medium below the boundary. Note that γ_{β} , γ_{M} are dimensionless parameters. A and D are also dimensionless parameters given by:

$$A = \left[\frac{\gamma_{M1}}{(\gamma_{M1})^{2} + \gamma_{\beta 1}} - \frac{\gamma_{M2}}{(\gamma_{M2})^{2} + \gamma_{\beta 2}}\right] \frac{2Z_{1}Z_{2}}{Z_{1} + Z_{2}};$$
$$D = \frac{Z_{1}Z_{2}\sqrt{\gamma_{\beta 1}\gamma_{\beta 2}}}{\gamma_{M1}\gamma_{M2}} \left[\frac{1}{\sqrt{\gamma_{\kappa}}} \frac{1}{\gamma_{\rho 2}} \frac{\upsilon_{b1}}{M_{1}} \sqrt{(\gamma_{M1})^{2} + \gamma_{\beta 1}} + \frac{1}{\gamma_{\rho 1}} \frac{\upsilon_{b2}}{M_{2}} \sqrt{(\gamma_{M2})^{2} + \gamma_{\beta 2}}\right]$$

where, γ_{κ} and γ_{ρ} are:

$$\gamma_{\kappa} = \frac{\varepsilon_2}{\varepsilon_1}$$
 and $\gamma_{\rho} = \frac{\rho_b}{\rho_f}$

 ρ_b is the bulk density and ρ_f is the density of the pore fluid.

Finally, K_{sg} and K_{fg} are given by:

$$K_{sg} = \frac{K_g}{1-\phi}$$
 and $K_{fg} = \frac{K_g}{1-\frac{K}{K_g}}$

 K_g is the bulk modulus of solid grain, K is the dry rock bulk modulus, and ϕ is porosity.

The asymptotic solutions provide approximations to Biot's theory, however, more explicit descriptions on the rock and fluid properties are obtained in asymptotic formulas. Table 1 summarizes the input parameters needed in this calculation. Where, K_g and ρ_g are the bulk modulus and density of the solid grain; K_{dry} and μ_{dry} are the dry rock bulk modulus and shear modulus; ϕ and κ are porosity and permeability of the rock; K_f , ρ_f , and η_f are the bulk modulus, density and viscosity of the filling fluid, respectively. Note that all these input parameters are no more than the ones used in doing a fluid substitution with Gassmann's equation. They can be easily acquired from log data. Therefore, wider applications of Biot's theory may be obtained through these asymptotic solutions. (Goloshubin et al., 2008).

Table 1. Input properties for asymptotic Biot's calculation.

Input prop.	Grain bulk mod.	Grain dens.	Dry rock bulk mod.	Dry rock shear mod.	Poro.	Perm.	Fluid bulk mod.	Fluid dens.	Fluid visco.
Symbol	Kg	$ ho_{g}$	K _{dry}	μ_{dry}	φ	к	\mathbf{K}_{f}	$ ho_{\mathrm{f}}$	η_{f}

Further more, velocity (m/s) and attenuation coefficients in units of (1/m) for Fast and Slow waves can be calculated from:

$$\begin{split} V^{F} &= v_{b}\sqrt{1 + \frac{\gamma_{M}^{2}}{\gamma_{\beta}}} + ...; \\ V^{S} &= v_{f}\sqrt{\frac{2|\varepsilon|}{\gamma_{\beta} + \gamma_{M}^{2}}} + ...; \\ a^{F} &= \frac{\omega}{v_{b}}\sqrt{\frac{\gamma_{\beta}}{\gamma_{\beta} + \gamma_{M}^{2}}} \frac{\zeta_{1}^{F}}{2\zeta_{0}^{F}}|\varepsilon| + ...; \\ a^{S} &= \frac{\omega}{v_{f}}\sqrt{\frac{\gamma_{\beta} + \gamma_{M}^{2}}{2|\varepsilon|}} + ...; \end{split}$$

where,
$$v_f = \sqrt{\frac{M}{\rho_f}}$$
, and ζ_0^F, ζ_1^F are given by:

$$\varsigma_0^F = \frac{\gamma_M^2 + \gamma_\beta}{\gamma_\beta \gamma_\rho}, \text{ and } \varsigma_1^F = \frac{1}{\gamma_\beta (\gamma_M^2 + \gamma_\beta)} (\frac{\gamma_M^2 + \gamma_\beta}{\gamma_\rho} - \gamma_M)^2$$

2.2 Biot's Slow wave as incident wave

Asymptotic solution obtains the reflection and transmission coefficients from incident Slow wave converts to both Fast P wave and Slow waves as follows:

$$R^{SS} = \frac{-\chi_{01}^{S} \frac{1}{\sqrt{\gamma_{\kappa}}} M_{2} k_{02}^{S} \xi_{02}^{S} + \chi_{02}^{S} M_{1} k_{01}^{S} \xi_{01}^{S}}{\chi_{01}^{S} \frac{1}{\sqrt{\gamma_{\kappa}}} M_{2} k_{02}^{S} \xi_{02}^{S} + \chi_{02}^{S} M_{1} k_{01}^{S} \xi_{01}^{S}};$$

$$T^{SS} = \frac{\chi_{02}^{S} \frac{1}{\sqrt{\gamma_{\kappa}}} M_{2} k_{02}^{S} \xi_{02}^{S} + \chi_{01}^{S} M_{1} k_{01}^{S} \xi_{01}^{S}}{\chi_{01}^{S} \frac{1}{\sqrt{\gamma_{\kappa}}} M_{2} k_{02}^{S} \xi_{02}^{S} + \chi_{02}^{S} M_{1} k_{01}^{S} \xi_{01}^{S}};$$

$$R^{SF} = \frac{Z_{2}(-1 - R^{SS} + T^{SS})}{Z_{1} + Z_{2}};$$

$$T^{SF} = \frac{-Z_{1}(-1 - R^{SS} + T^{SS})}{Z_{1} + Z_{2}},$$

$$k_{0}^{S} = \frac{1}{\sqrt{\gamma_{\beta} + \gamma_{M}^{2}}}, \quad \chi_{0}^{S} = \frac{\gamma_{M}^{2} + \gamma_{\beta}}{Z_{1} + Z_{2}} \text{ and } \xi_{0}^{S} = -\frac{1}{2}.$$

where,
$$k_0^s = \frac{1}{v_f} \sqrt{\gamma_\beta + \gamma_M^2}$$
, $\chi_0^s = \frac{\gamma_M^s + \gamma_\beta}{\gamma_M}$ and $\xi_0^s = -\frac{1}{\gamma_M}$

2.3 Asymptotic calculation on gas-water contact

In the first calculation using asymptotic formulas of Biot, we use the gas-water contact model, i.e., a gas sand overlying a water sand, while the rock properties for both the gas zone and water zone are kept same. For comparison purpose, all the properties are taken from Dutta & Ode (1983) for unconsolidated, Texas Gulf coast sand at depth of about 1500 m, as shown in Table 2.

Input prop.	Grain bulk mod.	Grain dens.	Dry rock bulk mod.	Dry rock shear mod.	Poro.	Perm.	Fluid bulk mod.	Fluid dens.	Fluid visco.
Symbol	Kg (Gpa)	$ ho_{g}$ (g/cc)	K _{dry} (Gpa)	μ _{dry} (Gpa)	φ	к (darcy)	K _f (Gpa)	$\rho_{\rm f}$ (g/cc)	η _f (cp)
Gas zone	35	2.65	1.7	1.855	0.3	1	0.022	0.1	0.015
Water zone	35	2.65	1.7	1.855	0.3	1	2.4	1	1

Table 2. Rock and fluid properties of gas and water saturated sand.

2.3.1 Velocity versus frequency

The velocity versus frequency plot are displayed in Figure 2 for both P wave and Biot's Slow wave in gas layer and water layer, an extrapolated curve from Dutta & Ode is also plotted as a comparison to the Slow wave velocity from present calculation. P wave velocity for both water and gas layers stay as constant through out the $10 \sim 10^5$ Hz frequency range, while a strong velocity dispersion is calculated for the Slow wave, both in water and gas layers. In the low seismic frequency range ($10 \sim 100$ Hz), the asymptotic calculations show good agreement with exact Biot's calculation of Dutta and Ode (1983).



Figure 2. Velocity dispersion of the P wave and Biot's Slow wave in gas and water saturated porous rocks.

2.3.2 Attenuation versus frequency

The attenuation of the P wave and Biot's Slow wave in water and gas saturated rocks are displayed in Figure 3. The attenuation of Biot's Slow wave is about 10^5 times greater than that for the Fast P wave at the seismic frequency range. By comparing the curves of asymptotic calculations (blue) and Dutta & Ode's exact Biot's calculations (red), strong similarities are found for both gas and water saturated rocks at low frequencies below 10^3 Hz. High frequencies, on the other hand, proved to have a low agreement between these two calculations. Attenuation of P wave is tiny with respect to the attenuation of Slow wave, however in a fluid saturated zone, the attenuation of P wave is enhanced by a mechanism of conversion to Biot's Slow wave. Studies of Dutta & Ode (1979a, b) and Dutta & Seriff (1979) have showed this trend. Asymptotic calculations provide similar results with their studies in terms of attenuation.

Lists of reflection and transmission coefficients for up and down going waves at 22 Hz are summarized in Table 3. Reflection coefficient of Fast P wave to Slow wave (Rfs) in water sand (equals to 0.025977), is much larger than the reflection coefficient (Rfs) in gas sand (equals to -0.000105); transmission coefficient of Fast P wave to Slow wave (Tfs) from gas sand to water sand (equals to -0.003897), is much larger than the transmission coefficient (Tfs) from water sand to gas sand (equals to 0.000697). This suggests that the amplitude of Slow P wave always increases going from gas zone to water zone, and decreases going from water zone to gas zone. Slow P wave needs relatively incompressible fluid to support it.

Table 3. Results of asymptotic calculations at 22 Hz on reflection and transmission coefficients for up and down going waves at the gas-water contact shows in Table 2.

Wave Type	P incidence Down going	Slow incidence Down going	P incidence Up going	Slow incidence Up going
Reflection to P wave	-0.263028	0.453893	0.251292	-0.444078
Reflection to Slow wave	-0.000105	-0.960673	0.025977	0.960673
Transmission to P wave	0.740764	-0.266208	1.276572	0.757167
Transmission to Slow wave	-0.003897	0.759428	0.000697	0.759428



Figure 3. Attenuation coefficients vs. Frequency and comparison with Dutta & Ode's calculations.

According to Table 3, the largest value of the coefficient for conversion from Fast P wave to Slow P wave is the reflection from water sand to water sand (equals to 0.02597). This amount is similar to Dutta & Ode's (1983) study, that they observed 2.5% of energy loss due to mod conversion from P wave to Slow wave. Since Slow P wave attenuates fast, most of the Slow wave energy would dissipate through fluid oscillations.

Therefore, from the comparisons of velocity and attenuation, asymptotic calculation provides similar results with exact Biot's solution at seismic frequency range. Since asymptotic calculation simplifies the algorithm of Biot's theory and relates the model more explicitly with rock and fluid properties, it can be more practically used as a tool for seismic inversion, simulation and reservoir characterization, etc.

2.3.3 Reflections versus frequency

The reflection and transmission coefficients for Fast P wave as an incident wave entering from gas zone onto a gas-water contact are displayed in Figure 4. Both the conversion to Fast P wave and Biot's Slow wave are plotted. Reflection (Rff) and transmission coefficient (Tff) are compared with the results from classical elastic calculations. We can see a significant frequency dependency of the Rff and Tff, while the classical Rff and Tff are not dependent on frequency. The polarity in our reflection coefficient is from European convention. A negative reflection coefficient exists for wave goes from low impedance rock to high impedance rock. Phase angle in degrees for Rff, Tff, Rfs, and Tfs are also plotted as a function of frequency. As frequency increases, phase angle increases for Rff and Tff. Rff phase increases faster than that for Tff phase, but generally small phase angles being less than 5 degrees are observed for both Rff and Tff within seismic frequency range. Since Rfs and Tfs only have first order term with respect to frequency in asymptotic formulas, their phase stays as a constant throughout all frequency range.

In Table 4, the 100 Hz and 10 KHz results from asymptotic calculations and from Dutta & Ode's calculations at normal incidence are summarized. Correct the polarity difference between asymptotic calculation and Dutta & Ode's calculation, their values for Rff and Tff are very close at 100 Hz. At 10 KHz, both values for Rff and Tff are very different. According to the comparison for velocity and attenuation, asymptotic calculation will no longer match with exact Biot's calculations for high frequency above 1 KHz, the relative big deviation at 10 KHz can be expected. This comparison further proves that Asymptotic calculation matches with the exact Biot's calculation at seismic frequency domain, thus it can be used for modeling and analysis to seismic data.



Figure 4. Reflection and transmission coefficients and phase angle for the wave propagation at the gaswater contact in Table 2. Incident wave is from gas sand.

Table 4. Comparison between asymptotic calculations and Dutta & Ode's calculations on the reflection and transmission coefficients (Rff and Tff) for the gas-water contact in Table 2, normal incidence.

Frequency	100	Hz	10 K	10 KHz		
Туре	Rff	Tff	Rff	Tff		
Asymptotic	0.241	0.742	0.061	0.769		
Dutta & Ode	0.246	0.744	0.175	0.690		

CHAPTER 3: Modeling Multi-layered Media

3.1 Propagator matrix method

In this section, we derive the classical propagator matrix method to obtain 1-D reflectivity and transmitivity at a single frequency for multi-layered fluid-saturated porous permeable media. Calculation is only for fluid zone and assumption is that both source and receiver are located at the half space. Robinson (1967) provided a good demonstration on applying propagator matrix method to solve P wave propagation in layered media with z-transform. More general description of this method is presented in Aki & Richards (1980). Here we modified the algorithm to include the mod conversion between P wave and Biot's Slow wave at normal incidence.

Figure 5 shows a boundary condition of the Fast and Slow P-waves traveling vertically at an arbitrary layer *j*. The ray paths are drawn with time displacement along the horizontal axis, which helps in displaying the vertically traveling rays through time axis. Indeed, all the ray paths are perpendicular to the horizontal plane. In our treatment, each layer is assumed to have same one-way travel time for P wave propagating through one layer. And this one-way travel time is taken to be one unit of time for Fast P wave; and τ unit of time for Slow P wave. The τ value

changes from layer to layer, depends on the ratio of the velocities of Fast P wave *vfast* and Slow P wave *vslow*. Namely, for an arbitrary layer *j*, we have:

$$\tau_j = \frac{v fast_j}{v slow_j}.$$

In Figure 5, we denote the downgoing Fast P wave at the top of layer *j* by $d_j(t)$, and the downgoing Slow wave at the top of layer *j* by $d_j'(t)$. Then, if there is no attenuation in layer *j*, the downgoing wave at the bottom of layer *j* will be the same waveform delayed by the one-way travel time for the layer *j* (which is defined as one time unit for Fast P wave, and τ time unit for Slow P wave); hence the downgoing Fast P wave at the bottom of layer *j* is $d_j(t-1)$, the downgoing Slow P wave at the bottom of layer *j* is $d_j'(t-\tau)$. Similarly, we denote the upgoing Fast P wave at the top of layer *j* by $u_j(t)$, and the upgoing Slow P wave at the top of layer *j* by $u_j'(t)$. Then the upgoing Fast P wave at the bottom of layer *j* is the same wave but advanced by one time unit, i.e., $u_j(t+1)$, and the upgoing Slow P wave at the bottom of layer *j* is $u_i'(t+\tau)$.



Figure 5. Schematic plot of wave propagation through layer j at normal incidence. The horizontal displacement corresponds to time.

If attenuation of waves in layer *j* is considered, then, the downgoing Fast P wave at the bottom of layer *j* becomes $A_f \cdot d_j(t-1)$, where A_f is the attenuation of P wave. The downgoing Slow P wave at the bottom of layer *j* becomes $A_s \cdot d_j$ '(*t*-1), where A_s is the attenuation of Slow wave. Similarly, the upgoing Fast P wave at the bottom of layer *j* becomes $A_f^{-1} \cdot u_j(t+1)$, and the upgoing Slow P wave at the bottom of layer *j* becomes $A_s^{-1} \cdot u_j$ '(*t*+ τ). The expressions of A_f and A_s are shown below:

$$A_{f} = \exp(-\alpha_{j}^{f}h_{j}) = \exp(-\alpha_{j}^{f}(vfast_{j} \cdot dt));$$
$$A_{s} = \exp(-\alpha_{j}^{s}h_{j}) = \exp(-\alpha_{j}^{s}(vfast_{j} \cdot dt)),$$

where, dt is the unit of time or sample time; α_j^s is the attenuation coefficient of Slow P wave and α_j^f is the attenuation coefficient of Fast P wave in units of (m⁻¹).

According to the boundary condition in Figure 5, we can obtain the relationships between all waveforms at interface *j* with the corresponding reflection and transmission coefficients. We use *rff* to represent the reflection coefficient of Fast P wave to Fast P wave while the incident P wave is downgoing, and *rffup* to represent the reflection coefficient of Fast P wave to Fast P wave while the incident P wave to Fast P wave while the incident Fast P wave while the incident are used for other reflection and transmission coefficients.

The wave $d_{j+1}(t)$ is made up of four parts, i.e., the parts due to transmitted portion of $d_j(t-1)$ and $d_j'(t-\tau)$, and the parts due to the reflected portion of $u_{j+1}(t)$ and $u_{j+1}'(t)$. Thus it gives the equation:

$$d_{j+1}(t) = tff_j \cdot A_f \cdot d_j(t-1) + tsf_j \cdot A_s \cdot d'_j(t-\tau_j) + rffup_j \cdot u_{j+1}(t) + rsfup_j \cdot u'_{j+1}(t),$$

Similarly the wave $d_{j+1}'(t)$ is made up of four parts, i.e., the transmitted portion of $d_j(t-1)$ and $d_j'(t-\tau)$, and the reflected portion of $u_{j+1}(t)$ and $u_{j+1}'(t)$. Thus we have the equation:

$$d'_{j+1}(t) = tfs_{j} \cdot A_{f} \cdot d_{j}(t-1) + tss_{j} \cdot A_{s} \cdot d'_{j}(t-\tau_{j}) + rfsup_{j} \cdot u_{j+1}(t) + rssup_{j} \cdot u'_{j+1}(t).$$

Similarly the waves $u_j(t+1)$ and $u_j'(t+\tau)$ are made up of four parts, i.e., the reflected portion of $d_j(t-1)$ and $d_j'(t-\tau)$, and the transmitted portion of $u_{j+1}(t)$ and $u_{j+1}'(t)$. Thus we have the equations:

$$A_{f}^{-1} \cdot u_{j}(t+1) = rff_{j} \cdot A_{f} \cdot d_{j}(t-1) + rsf_{j} \cdot A_{s} \cdot d'_{j}(t-\tau_{j}) + tffup_{j} \cdot u_{j+1}(t) + tsfup_{j} \cdot u'_{j+1}(t);$$

$$A_{s}^{-1} \cdot u'_{j}(t+\tau_{j}) = rfs_{j} \cdot A_{f} \cdot d_{j}(t-1) + rss_{j} \cdot A_{s} \cdot d'_{j}(t-\tau_{j}) + tfsup_{j} \cdot u_{j+1}(t) + tssup_{j} \cdot u'_{j+1}(t).$$

We define $D_j(s)$ as the Laplace transform of $d_j(t)$, i.e.,

$$D_j(s) = \int_0^\infty d_j(t) e^{-st} dt \cdot$$

 $D_i(s)$ represents all the downgoing waveforms at the top of layer *j*.

The Laplace transform of $d_i(t-1)$ is

$$\int_{0}^{\infty} d_{j}(t-1)e^{-st}dt = \int_{0}^{\infty} d_{j}(t_{1})e^{-s(t_{1}+1)}dt_{1},$$

If we define $z = e^{-s}$, then,

$$\int_{0}^{\infty} d_{j}(t-1)e^{-st}dt = z^{1}D_{j}(s).$$

 $z^{1}D_{j}(s)$ represents all the downgoing waveforms at the bottom of layer *j*.

Thus, in Laplace transform, the waveform at the bottom of layer *j* differs with the one at the top of layer *j* by a multiplication of z^1 . We can also view $D_j(s)$ as a polynomial of z, then, the multiplication of $D_j(s)$ by z^1 corresponds to a shift of the polynomial of $D_j(s)$ by one step to the right. Also the multiplication of two waveforms in Laplace transform is equivalent to a convolution of their polynomial coefficients in z. These characters are very useful in doing subsequent polynomial operations.

Similarly, we can find the Laplace transforms for other waves in above equations and construct four new equations in Laplace transforms, namely:

$$D_{j+1}(s) = tff_{j} \cdot A_{f} \cdot z^{1}D_{j}(s) + tsf_{j} \cdot A_{s} \cdot z^{\tau_{j}}D_{j}'(s) + rffup_{j} \cdot U_{j+1}(s) + rsfup_{j} \cdot U_{j+1}'(s);$$

$$D_{j+1}'(s) = tfs_{j} \cdot A_{f} \cdot z^{1}D_{j}(s) + tss_{j} \cdot A_{s} \cdot z^{\tau_{j}}D_{j}'(s) + rfsup_{j} \cdot U_{j+1}(s) + rssup_{j} \cdot U_{j+1}'(s);$$

$$A_{f}^{-1} \cdot z^{-1}U_{j}(s) = rff_{j} \cdot A_{f} \cdot z^{1}D_{j}(s) + rsf_{j} \cdot A_{s} \cdot z^{\tau_{j}}D_{j}'(s) + tffup_{j} \cdot U_{j+1}(s) + tsfup_{j} \cdot U_{j+1}'(s);$$

$$A_{s}^{-1} \cdot z^{-\tau_{j}}U_{j}'(s) = rfs_{j} \cdot A_{f} \cdot z^{1}D_{j}(s) + rss_{j} \cdot A_{s} \cdot z^{\tau_{j}}D_{j}'(s) + tfsup_{j} \cdot U_{j+1}(s) + tssup_{j} \cdot U_{j+1}'(s).$$

Rearrangement of the above equations leads to the following four equations:

$$D_{j+1}(s) = tff_j \cdot A_f \cdot z^1 D_j(s) + tsf_j \cdot A_s \cdot z^{\tau_j} D_j'(s) + rffup_j \cdot U_{j+1}(s) + rsfup_j \cdot U_{j+1}'(s)$$
(1)

$$D'_{j+1}(s) = tfs_{j} \cdot A_{f} \cdot z^{1}D_{j}(s) + tss_{j} \cdot A_{s} \cdot z^{\tau_{j}}D'_{j}(s) + rfsup_{j} \cdot U_{j+1}(s) + rssup_{j} \cdot U'_{j+1}(s)$$
(2)

$$U_{j+1}(s) = \frac{-rff_{j}}{tffup_{j}} \cdot A_{f} \cdot z^{1}D_{j}(s) + \frac{-rsf_{j}}{tffup_{j}} \cdot A_{s} \cdot z^{\tau_{j}}D_{j}(s) + \frac{-tsfup_{j}}{tffup_{j}} \cdot U_{j+1}(s) + \frac{1}{tffup_{j}} \cdot A_{f}^{-1} \cdot z^{-1}U_{j}(s)$$
(3)

$$U_{j+1}(s) = \frac{-rfs_{j}}{tssup_{j}} \cdot A_{f} \cdot z^{1}D_{j}(s) + \frac{-rss_{j}}{tssup_{j}} \cdot A_{s} \cdot z^{\tau_{j}}D_{j}(s) + \frac{-tfsup_{j}}{tssup_{j}} \cdot U_{j+1}(s) + \frac{1}{tssup_{j}} \cdot A_{s}^{-1} \cdot z^{-\tau_{j}}U_{j}(s)$$
(4)

Substituting equation (4) into equation (3) leads to:

$$U_{j+1}(s) = \frac{-tssup_{j} \cdot rff_{j} + tsfup_{j} \cdot rfs_{j}}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}} \cdot A_{f} \cdot z^{1}D_{j}(s) + \frac{-tssup_{j} \cdot rsf_{j} + tsfup_{j} \cdot rss_{j}}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}} \cdot A_{s} \cdot z^{\tau_{j}}D_{j}(s) + \frac{tssup_{j}}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}} \cdot A_{s} \cdot z^{\tau_{j}}D_{j}(s) + \frac{tssup_{j}}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}} \cdot A_{s}^{-1} \cdot z^{-\tau_{j}}U_{j}(s) + \frac{19}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}} \cdot A_{s}^{-1} \cdot z^{-\tau_{j}}U_{j}(s)$$

Substituting equation (5) into equation (4) leads to:

$$U_{j+1}(s) = \frac{-rfs_{j} \cdot tffup_{j} + rff_{j} \cdot tfsup_{j}}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}} \cdot A_{f} \cdot z^{1}D_{j}(s) + \frac{-rss_{j} \cdot tffup_{j} + rsf_{j} \cdot tfsup_{j}}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}} \cdot A_{s} \cdot z^{\tau_{j}}D_{j}(s) + \frac{-tfsup_{j}}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}} \cdot A_{s}^{-1} \cdot z^{-\tau_{j}}U_{j}(s) + \frac{tffup_{j}}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}} \cdot A_{s}^{-1} \cdot z^{-\tau_{j}}U_{j}(s)$$

$$(6)$$

Substituting equation (5) and equation (6) into equation (1) leads to:

$$D_{j+1}(s) = \left[\frac{tff_{j} \cdot (tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}) + rffup_{j} \cdot (-tssup_{j} \cdot rff_{j} + tsfup_{j} \cdot rfs_{j})}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}}\right] \cdot A_{f} \cdot z^{1}D_{j}(s) + \frac{rsfup_{j} \cdot (-rfs_{j} \cdot tffup_{j} + rff_{j} \cdot tfsup_{j})}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}}\right] \cdot A_{f} \cdot z^{1}D_{j}(s) + \left[\frac{tsf_{j} \cdot (tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}) + rffup_{j} \cdot (-tssup_{j} \cdot rsf_{j} + tsfup_{j} \cdot rss_{j})}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}}\right] \cdot A_{s} \cdot z^{\tau_{j}}D_{j}(s) + \frac{rffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}}\right] \cdot A_{s} \cdot z^{\tau_{j}}D_{j}(s) + \frac{rffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}} \cdot A_{s}^{-1} \cdot z^{-\tau_{j}}U_{j}(s)$$

Substituting equation (5) and equation (6) into equation (2) leads to:

$$D_{j+1}^{'}(s) = \left[\frac{tfs_{j} \cdot (tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}) + rfsup_{j} \cdot (-tssup_{j} \cdot rff_{j} + tsfup_{j} \cdot rfs_{j})}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}}\right] \cdot A_{f} \cdot z^{1}D_{j}(s) + \frac{rssup_{j} \cdot (-rfs_{j} \cdot tffup_{j} + rff_{j} \cdot tfsup_{j})}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}}\right] \cdot A_{f} \cdot z^{1}D_{j}(s) + \left[\frac{tss_{j} \cdot (tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}) + rfsup_{j} \cdot (-tssup_{j} \cdot rsf_{j} + tsfup_{j} \cdot rss_{j})}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}}\right] \cdot A_{s} \cdot z^{\tau_{j}}D_{j}(s) + \frac{rfsup_{j} \cdot (-rss_{j} \cdot tffup_{j} + rsf_{j} \cdot tfsup_{j})}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}}\right] \cdot A_{s} \cdot z^{\tau_{j}}D_{j}(s) + \frac{rfsup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tsfup_{j} + rssup_{j} \cdot tfsup_{j}}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}} \cdot A_{s}^{-1} \cdot z^{-\tau_{j}}U_{j}(s)$$

According to equation (7), (8), (5) and (6), a simple matrix form can be obtained:

$$\begin{bmatrix} D_{j+1}(s) \\ D_{j+1}^{'}(s) \\ U_{j+1}(s) \\ U_{j+1}^{'}(s) \end{bmatrix} = \frac{z^{-\tau_{j}}}{tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}} \cdot \begin{bmatrix} M_{j} \end{bmatrix}_{4\times 4} \cdot \begin{bmatrix} D_{j}(s) \\ D_{j}^{'}(s) \\ U_{j}(s) \\ U_{j}^{'}(s) \end{bmatrix},$$
(9)

here $[M_j]$ is the propagator matrix for Fast P wave and Slow P wave traveling vertically through a porous, permeable fluid-saturated layer *j*. The matrix element of $[M_j]$ can be found from equations (7), (8), (5) and (6), and are summarized in appendix 1. Thus given the asymptotic calculations of the reflection and transmission coefficients for each layer, we could recursively calculate all the downgoing and upgoing waveforms $D_j(s)$, $D_j'(s)$, $U_j(s)$ and $U_j'(s)$ in Laplace transforms from layer 0 to layer k+1, where layer 0 and layer k+1 are two half spaces (Figure 6).

source	
	layer 0
	layer 1
	layer 2
	layer k
	laver k+1

Figure 6. Schematic plot of the propagations of waves through multi-layered media from layer 0 to layer k+1.

From layer 1 to layer k+1, matrix propagation provides the following relation:

$$\begin{bmatrix} D_{k+1}(s) \\ D_{k+1}^{'}(s) \\ U_{k+1}(s) \\ U_{k+1}^{'}(s) \end{bmatrix} = \frac{z^{-\sum_{j=1}^{k} \tau_{j}}}{\prod_{j=1}^{k} (tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j})} \cdot M_{k} \dots M_{2}M_{1} \cdot \begin{bmatrix} D_{1}(s) \\ D_{1}^{'}(s) \\ U_{1}(s) \\ U_{1}^{'}(s) \end{bmatrix},$$

here, $M_1, M_2, ..., M_k$ are the propagator matrix of layer 1, 2,..., k.

If we assume that the source is placed on the surface, i.e., the bottom of layer 0, then there is no time delay from layer 0 to layer 1. Thus, by setting the time delay z = 1 in equation (9), we can obtain the waveforms from layer 0 to layer 1 by:

$$\begin{bmatrix} D_1(s) \\ D_1^{'}(s) \\ U_1(s) \\ U_1^{'}(s) \end{bmatrix} = \frac{1}{tffup_0 \cdot tssup_0 - tsfup_0 \cdot tfsup_0} \cdot M_0 \cdot \begin{bmatrix} D_0(s) \\ D_0^{'}(s) \\ U_0(s) \\ U_0^{'}(s) \end{bmatrix},$$

here, M_0 is the propagator matrix of layer 0. Together with the matrix propagation from layer 1 to layer k+1, we could derive a relation between the waveforms of layer 0 and layer k+1 by the following equation:

$$\begin{bmatrix} D_{k+1}(s) \\ D_{k+1}^{'}(s) \\ U_{k+1}(s) \\ U_{k+1}^{'}(s) \end{bmatrix} = \frac{z^{-\sum_{j=1}^{k} \tau_{j}}}{\prod_{j=0}^{k} (tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j})} \cdot \prod_{j=0}^{k} M_{j} \cdot \begin{bmatrix} D_{0}(s) \\ D_{0}^{'}(s) \\ U_{0}(s) \\ U_{0}^{'}(s) \end{bmatrix} = C \cdot N_{k} \cdot \begin{bmatrix} D_{0}(s) \\ D_{0}^{'}(s) \\ U_{0}(s) \\ U_{0}^{'}(s) \end{bmatrix},$$

where,

$$C = \frac{z^{-\sum_{j=1}^{k} \tau_{j}}}{\prod_{j=0}^{k} (tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j})} ; \text{ and } N_{k} = \prod_{j=0}^{k} M_{j}.$$

Matrix M_j and M_0 have the following forms and the explicit expressions can be found in appendix 1:

$$M_{j} = \begin{bmatrix} M_{j}(1,1) & M_{j}(1,2) & M_{j}(1,3) & M_{j}(1,4) \\ M_{j}(2,1) & M_{j}(2,2) & M_{j}(2,3) & M_{j}(2,4) \\ M_{j}(3,1) & M_{j}(3,2) & M_{j}(3,3) & M_{j}(3,4) \\ M_{j}(4,1) & M_{j}(4,2) & M_{j}(4,3) & M_{j}(4,4) \end{bmatrix},$$

and,

$$M_{0} = \begin{bmatrix} M_{0}(1,1) & M_{0}(1,2) & M_{0}(1,3) & M_{0}(1,4) \\ M_{0}(2,1) & M_{0}(2,2) & M_{0}(2,3) & M_{0}(2,4) \\ M_{0}(3,1) & M_{0}(3,2) & M_{0}(3,3) & M_{0}(3,4) \\ M_{0}(4,1) & M_{0}(4,2) & M_{0}(4,3) & M_{0}(4,4) \end{bmatrix}.$$

3.2 Reflectivity and transmitivity series

We already obtained the matrix propagation from layer 0 to layer k+1, thus we have the equation below:

$$\begin{bmatrix} D_{k+1}(s) \\ D_{k+1}^{'}(s) \\ U_{k+1}(s) \\ U_{k+1}^{'}(s) \end{bmatrix} = C \cdot N_{k} \cdot \begin{bmatrix} D_{0}(s) \\ D_{0}^{'}(s) \\ U_{0}(s) \\ U_{0}^{'}(s) \end{bmatrix} = C \cdot \begin{bmatrix} N_{k}(1,1) & N_{k}(1,2) & N_{k}(1,3) & N_{k}(1,4) \\ N_{k}(2,1) & N_{k}(2,2) & N_{k}(2,3) & N_{k}(2,4) \\ N_{k}(3,1) & N_{k}(3,2) & N_{k}(3,3) & N_{k}(3,4) \\ N_{k}(4,1) & N_{k}(4,2) & N_{k}(4,3) & N_{k}(4,4) \end{bmatrix} \cdot \begin{bmatrix} D_{0}(s) \\ D_{0}^{'}(s) \\ U_{0}^{'}(s) \\ U_{0}^{'}(s) \end{bmatrix},$$

where, matrix N_k is obtained by recursive multiplication of propagator matrix M_0 through M_k , i.e.,

$$N_k = M_k \dots M_1 \cdot M_0 = \prod_{j=0}^k M_j.$$

Note that each matrix element of propagator matrix M_j is a polynomial in z(Appendix 1), for example, $M_j(1,3) = (rffup_j \cdot tssup_j - rsfup_j \cdot tfsup_j) \cdot A_j^{-1} \cdot z^{\tau_j - 1}$, which has only $(\tau_j$ -1)-th order term in z polynomial. And notice that the highest order non-zero term in matrix M_j has $(2\tau_j)$ -th order, they are $M_j(1,2)$, $M_j(2,2)$, $M_j(3,2)$ and $M_j(4,2)$, thus we can define an array with length of $(2\tau_j+1)$ to represent the matrix element of M_j , where the first value of the array corresponds to the zero order term in z polynomial, and the $(2\tau_j+1)$ -th value of the array corresponds to the $(2\tau_j)$ -th order term in z polynomial. The multiplication of each matrix element of M_j is equivalent to convolution of its corresponding arrays. Thus, all the matrix operations can be applied to our matrix propagation process except for replacing the multiplication of matrix elements by a convolution of the corresponding arrays.

The impulse input corresponds to a downgoing Fast P wave with amplitude equals to 1, i.e., $D_0(s) = 1$ and we assume there is no input Slow P wave, thus, D_0 ' = 0. And there are also no upgoing waveforms from the bottom half space (layer k+1), thus, $U_{k+1} = 0$ and U_{k+1} ' = 0. This gives:

$$\begin{bmatrix} D_{k+1}(s) \\ D_{k+1}^{'}(s) \\ 0 \\ 0 \\ 0 \end{bmatrix} = C \cdot N_{k} \cdot \begin{bmatrix} D_{0}(s) \\ D_{0}^{'}(s) \\ U_{0}(s) \\ U_{0}^{'}(s) \end{bmatrix} = C \cdot \begin{bmatrix} N_{k}(1,1) & N_{k}(1,2) & N_{k}(1,3) & N_{k}(1,4) \\ N_{k}(2,1) & N_{k}(2,2) & N_{k}(2,3) & N_{k}(2,4) \\ N_{k}(3,1) & N_{k}(3,2) & N_{k}(3,3) & N_{k}(3,4) \\ N_{k}(4,1) & N_{k}(4,2) & N_{k}(4,3) & N_{k}(4,4) \end{bmatrix} \cdot \begin{bmatrix} 1 \\ 0 \\ U_{0}(s) \\ U_{0}^{'}(s) \end{bmatrix}$$

Expand the above equation, we have:

$$\begin{cases} 0 = N_k(3,1) + N_k(3,3) \cdot U_0(s) + N_k(3,4) \cdot U_0'(s) \\ 0 = N_k(4,1) + N_k(4,3) \cdot U_0(s) + N_k(4,4) \cdot U_0'(s) \end{cases}.$$

Solve these two equations for $U_0(s)$ and $U_0'(s)$, we obtain:

$$U_0(s) = \frac{N_k(4,4) \cdot N_k(3,1) - N_k(3,4) \cdot N_k(4,1)}{N_k(3,4) \cdot N_k(4,3) - N_k(3,3) \cdot N_k(4,4)}, \text{ and}$$
$$U_0'(s) = \frac{N_k(3,3) \cdot N_k(4,1) - N_k(3,1) \cdot N_k(4,3)}{N_k(3,4) \cdot N_k(4,3) - N_k(3,3) \cdot N_k(4,4)}.$$

 $U_0(s)$ and $U_0'(s)$ as polynomials of z, are the reflectivity series of P wave and Slow wave, respectively.

We also have the equation for $D_{k+1}(s)$ as follows:

$$D_{k+1}(s) = C \cdot [N_k(1,1) + N_k(1,3) \cdot U_0(s) + N_k(1,4) \cdot U_0(s)],$$

where,

$$C = \frac{z^{-\sum_{j=0}^{k} \tau_{j}}}{\prod_{j=0}^{k} (tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j})}$$

Substitute $U_0(s)$ and $U_0'(s)$ into this equation for $D_{k+1}(s)$, we obtain:

$$\begin{split} D_{k+1}(s) &= C \cdot \Bigg[\frac{N_k(1,1) \cdot N_k(3,4) \cdot N_k(4,3) - N_k(1,1) \cdot N_k(3,3) \cdot N_k(4,4)}{N_k(3,4) \cdot N_k(4,3) - N_k(3,3) \cdot N_k(4,4)} + \\ & \frac{N_k(1,3) \cdot N_k(4,4) \cdot N_k(3,1) - N_k(1,3) \cdot N_k(3,4) \cdot N_k(4,1)}{N_k(3,4) \cdot N_k(4,3) - N_k(3,3) \cdot N_k(4,4)} + \\ & \frac{N_k(1,4) \cdot N_k(3,3) \cdot N_k(4,1) - N_k(1,4) \cdot N_k(3,1) \cdot N_k(4,3)}{N_k(3,4) \cdot N_k(4,3) - N_k(3,3) \cdot N_k(4,4)} \Bigg]. \end{split}$$

 $D_{k+1}(s)$ as a polynomial of z is the transmitivity series of the impulse P wave propagating through a multi-layered media.

3.2 Results of calculations

Figure 7 shows the reflectivity series vs. frequency from seven layers of rock with inhomogeneous fluid saturation (Table 5) and Figure 8 shows the same plot for a homogeneous fluid saturation with slightly different rock properties (Table 6). We can see a remarkable influence of the Slow P wave for the rock with inhomogeneous fluid saturation, while for the rock with homogeneous fluid saturation, while for the rock with homogeneous fluid saturation Slow P wave effect is very small. This is consistent with previous studies (Dutta & Ode, 1979a, b; Carcione et al., 2003).

It should be noted that previous studies recognized the high attenuation in the inhomogeneous fluid-saturated rock is due to the energy flow to Slow P wave, while in our case, the signal from mode conversion to Slow P wave is directly calculated.

Also, we can see in general the lower frequency signals last longer than higher frequencies. This phenomenon is similar to the low frequency shadows that are often observed beneath gas reservoirs. Since gas reservoir would introduce some degree of inhomogeneity in fluid saturation, such as gas bubbles. According to Figure 5, we think Slow wave may be a major cause for the low frequency shadows.

Grain bulk modulus	Grain density	Dry rock bulk modulus	Dry rock shear modulus	Porosity	Permeab.	Fluid bulk modulus	Fluid density	Fluid visc- osity
K _g [Gpa]	ρ _g [g/cc]	K _{dry} [Gpa]	μ _{dry} [Gpa]	ф	к [darcy]	K _f [Gpa]	ρ _f [g/cc]	η _f [cp]
38	2.65	1.46	1.56	0.3	2	0.025	0.15	0.01
38	2.65	1.46	1.56	0.3	2	2.42	1	1
38	2.65	1.46	1.56	0.3	2	0.025	0.15	0.01
								•••
38	2.65	1.46	1.56	0.3	2	0.025	0.15	0.01

Table 5. Input rock and fluid properties. Rock properties are the same for each layer, while fluid properties are changed alternatively between gas and water. Layer thickness equals to 0.1 ms for P wave.



Figure 7. Reflectivity series vs. frequency from seven layers of porous permeable sands with gas and water saturated alternatively (Table 5).



Figure 8. Reflectivity series vs. frequency from seven layers of porous permeable sands with only water saturation (Table 6).

Grain bulk modulus	Grain density	Dry rock bulk modulus	Dry rock shear modulus	Porosity	Permeab.	Fluid bulk modulus	Fluid density	Fluid visco- sity
K _g [Gpa]	$ ho_{g}$ [g/cc]	K _{dry} [Gpa]	μ _{dry} [Gpa]	ф	к [darcy]	K _f [Gpa]	ρ _f [g/cc]	η _f [cp]
38	2.65	1.46	1.56	0.3	2	2.42	1	1
35	2.65	1.7	1.855	0.1	0.1	2.42	1	1
38	2.65	1.46	1.56	0.3	2	2.42	1	1
38	2.65	1.46	1.56	0.3	2	2.42	1	1

Table 6. Input rock and fluid properties. Fluid properties are the same for each layer, rock properties are changed alternatively. Layer thickness equals to 0.1 ms for P wave.

The number of very thin fluid-saturated permeable layers has also effect on the seismic response. Figure 9 shows reflectivity series from nine layers of alternative gas/water sands, we can see that the seismic signal is enhanced as compared to Figure 7.



Figure 9. Same with Figure 7, only the number of total layers equals to nine.

In conclusion we would like to mark: 1) low frequency asymptotic description of the Biot's model was applied based on matrix propagator technique; 2) the asymptotic description provides accurate calculations at seismic frequencies; 3) Slow P wave effect strongly depends on frequency and in case of a reservoir with high permeability and inhomogeneous fluid saturation the Slow P wave effect must be taken into account.

CHAPTER 4: Future Directions

4.1 Improvement of propagator matrix method

Although the basic theory and matrix element of the propagator matrix for Fast-Slow P wave conversion have been derived, numerical instability due the limitation of the computer precision will lead to very serious problems. These problems make the application of the Propagator Matrix method only suitable for very thin layer and high permeable rocks. Jocker et al (2004) studied the numerical instability for propagator matrix method applied to Biot's model. In order to solve this numerical instability problem, some modification on the algorithm is needed. Studies of Dunkin (1965), Schmidt and Tango (1986), Levesque and Piche (1992) suggested some modification methods. Thus, to improve the numerical stability of the propagator matrix method applied in this study can be one of the future directions.

4.2 Permeability attributes

Based on the Asymptotic algorithm in Goloshubin and Silin (2005), a relative permeability attribute has been derived and applied on seismic data analysis. In Focus software version 5.4, PERMATR module allows users to convert the seismic amplitude traces into relative permeability traces. Examples of how PERMATR works are shown in Figure 10 and Figure 11. The seismic data is from South Marsh, Gulf of Mexico. There is a water well (SM_238_88) located at INLINE 2170, XLINE 1033. We can see the reservoir zone at about 2.7 second from Figure 10 and Figure 11. The high permeable sand is more apparent from the relative permeability traces. Thus, another possible future project can be on mapping of the high permeability zone from seismic data using PERMATR module, convert the seismic amplitude trace into permeability trace and find out the difference between them.

Future project related to this permeability attribute can also be trying to improve the permeability attributes and make it more reliable and more accurate.





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Appendix 1: Matrix Elements of M_j and M_0

$$\begin{split} M_{j}(\mathbf{l},\mathbf{l}) &= [tff_{j} \cdot (tflup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j}) + rffup_{j} \cdot (-tssup_{j} \cdot rff_{j} + tsfup_{j} \cdot rfs_{j}) + \\ &\quad rsfup_{j} \cdot (-rfs_{j} \cdot tfflup_{j} + rsf_{j} \cdot tfsup_{j})] \cdot A_{j} \cdot z^{\tau_{j}+1} \\ M_{j}(\mathbf{l},2) &= [tsf_{j} \cdot (tflup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j})] \cdot A_{s} \cdot z^{2\tau_{j}} \\ M_{j}(\mathbf{l},3) &= (rffup_{j} \cdot tssup_{j} - rsfup_{j} \cdot tfsup_{j}) \cdot A_{s}^{-1} \cdot z^{\tau_{j}-1} \\ M_{j}(\mathbf{l},4) &= (-rffup_{j} \cdot tssup_{j} - rsfup_{j} \cdot tfgup_{j}) \cdot A_{s}^{-1} \cdot 1 \\ M_{j}(\mathbf{l},4) &= (-rffup_{j} \cdot tsgup_{j} + rsfup_{j} \cdot tfgup_{j}) + rfsup_{j} \cdot (-tssup_{j} \cdot rff_{j} + tsfup_{j} \cdot rfs_{j}) + \\ &\quad rssup_{j} \cdot (-rfs_{j} \cdot tffup_{j} + rsfup_{j} \cdot tfgup_{j}) + rfsup_{j} \cdot (-tssup_{j} \cdot rff_{j} + tsfup_{j} \cdot rfs_{j}) + \\ &\quad rssup_{j} \cdot (-rfs_{j} \cdot tffup_{j} + rff_{j} \cdot tfsup_{j})] \cdot A_{f} \cdot z^{\tau_{f}+1} \\ M_{j}(2,2) &= [tss_{j} \cdot (tffup_{j} \cdot tssup_{j} - tsfup_{j} \cdot tfsup_{j})] \cdot A_{s} \cdot z^{2\tau_{j}} \\ M_{j}(2,3) &= (rfsup_{j} \cdot tssup_{j} - rssup_{j} \cdot tfsup_{j}) \cdot A_{f}^{-1} \cdot z^{\tau_{f}-1} \\ M_{j}(2,3) &= (rfsup_{j} \cdot tsgup_{j} - rssup_{j} \cdot tfsup_{j}) \cdot A_{f}^{-1} \cdot z^{\tau_{f}-1} \\ M_{j}(3,1) &= (-rssup_{j} \cdot tgfu_{j} + rsf_{j} \cdot tfsup_{j}) \cdot A_{s}^{-1} \cdot 1 \\ M_{j}(3,2) &= (-rssup_{j} \cdot rff_{j} + tsfup_{j} \cdot rss_{j}) \cdot A_{s} \cdot z^{2\tau_{j}} \\ M_{j}(3,3) &= tssup_{j} \cdot A_{f}^{-1} \cdot z^{\tau_{f}-1} \\ M_{j}(3,4) &= -tsfup_{j} \cdot A_{s}^{-1} \cdot 1 \\ M_{j}(4,1) &= (-rfs_{j} \cdot tffup_{j} + rff_{j} \cdot tfsup_{j}) \cdot A_{j} \cdot z^{\tau_{j}+1} \\ M_{j}(4,2) &= (-rss_{j} \cdot tffup_{j} + rff_{j} \cdot tfsup_{j}) \cdot A_{s} \cdot z^{2\tau_{j}} \\ M_{j}(4,3) &= -tfsup_{j} \cdot A_{s}^{-1} \cdot 1 \\ M_{j}(4,4) &= tffup_{j} \cdot A_{s}^{-1} \cdot 1 \end{split}$$

$$\begin{split} &M_{0}(1,1) = tff_{0} \cdot (tffup_{0} \cdot tssup_{0} - tsfup_{0} \cdot tfsup_{0}) + rffup_{0} \cdot (-tssup_{0} \cdot rff_{0} + tsfup_{0} \cdot rfs_{0}) + \\ & rsfup_{0} \cdot (-rfs_{0} \cdot tffup_{0} + rff_{0} \cdot tfsup_{0}) \\ &M_{0}(1,2) = tsf_{0} \cdot (tffup_{0} \cdot tssup_{0} - tsfup_{0} \cdot tfsup_{0}) + rffup_{0} \cdot (-tssup_{0} \cdot rsf_{0} + tsfup_{0} \cdot rss_{0}) + \\ & rsfup_{0} \cdot (-rss_{0} \cdot tffup_{0} + rsf_{0} \cdot tfsup_{0}) \\ &M_{0}(1,3) = rffup_{0} \cdot tssup_{0} - rsfup_{0} \cdot tfsup_{0} \\ &M_{0}(1,4) = -rffup_{0} \cdot tsfup_{0} + rsfup_{0} \cdot tfsup_{0} \\ &M_{0}(2,1) = tfs_{0} \cdot (tffup_{0} \cdot tssup_{0} - tsfup_{0} \cdot tfsup_{0}) + rfsup_{0} \cdot (-tssup_{0} \cdot rff_{0} + tsfup_{0} \cdot rfs_{0}) + \\ & rssup_{0} \cdot (-rfs_{0} \cdot tffup_{0} + rsf_{0} \cdot tfsup_{0}) \\ &M_{0}(2,2) = tss_{0} \cdot (tffup_{0} \cdot tssup_{0} - tsfup_{0} \cdot tfsup_{0}) + rfsup_{0} \cdot (-tssup_{0} \cdot rsf_{0} + tsfup_{0} \cdot rss_{0}) + \\ & rssup_{0} \cdot (-rss_{0} \cdot tffup_{0} + rsf_{0} \cdot tfsup_{0}) \\ &M_{0}(2,3) = rfsup_{0} \cdot tssup_{0} - tsfup_{0} \cdot tfsup_{0} \\ &M_{0}(2,4) = -rfsup_{0} \cdot tsfup_{0} + rssup_{0} \cdot tffup_{0} \\ &M_{0}(3,1) = -tssup_{0} \cdot rsf_{0} + tsfup_{0} \cdot rss_{0} \\ &M_{0}(3,2) = -tssup_{0} \cdot rsf_{0} + tsfup_{0} \cdot rss_{0} \\ &M_{0}(3,3) = tssup_{0} \\ &M_{0}(4,1) = -rfs_{0} \cdot tffup_{0} + rff_{0} \cdot tfsup_{0} \\ &M_{0}(4,2) = -rss_{0} \cdot tffup_{0} + rsf_{0} \cdot tfsup_{0} \\ &M_{0}(4,3) = -tfsup_{0} \\ &M_{0}(4,4) = tffup_{0} \\ \end{array}$$

Appendix 2: Fortran Code

A2.1 Example input file

1								
3	22	0.000	13					
38	2.65	1.46	1.56	0.3	2	0.025	0.15	0.01
38	2.65	1.46	1.56	0.3	2	2.42	1	1
38	2.65	1.46	1.56	0.3	2	0.025	0.15	0.01

A2.2 Output file from the input above

Type 0, to see self-document file

nlayer	freq[]	Hz] d	lt[sec]	multi	ples			
3	100.00	0.0	00100	3	-			
kø	rhog k	drv u	drv pł	ni kar	nna kf	rhof	nf	
[Gna]		[Gna]	[Gna]	phi n b]	arcv [(Fnal [c	$\frac{11}{2}$	nl
25 000	12650	1 700	1 955	0 200		$\int pa \int [e$	0 100	0.015
35.000	2.030	1.700	1.033	0.300	1.000	0.022	0.100	0.015
35.000	2.650	1.700	1.855	0.300	1.000	2.400	1.000	1.000
			100					
Reflect	tivity Slo	w wave	192					
-	0.26573	3480453	34913					
	0.00000	000000	00000					
	0.23133	7490453	32081					
	0.00000	000000	00000					
	0.013404	1231628	81641					
		1231020						
	0.00000	000000	00000					
-								
Transm	itivity Sl	ow wav	re 267					
	0.961054	4614036	54452					
	0.00000)000000	00000					
	0.055685	5737009	6958					
	0.000000	000000	00000					
	0.003226	5560968	35689					
	0 00000	000000	00000					
	0.000000		00000					

.

A2.3 Fortran code (http://www.geosc.uh.edu/~yliu/slowave.for)

C		
C	slowave - c	calculates the 1-D impulse reflectivity and
С	t	ransmitivity series of the Biot's Fast P wave and Slow
С	F	wave propagations through the fluid-saturated porous
С	p	ermeable layered media.
C		
C	Input:	
C	nlayer	number of total layers
C	freq	frequency in [Hz]
C	dt	sample rate or sample time [sec]
C	mtps	number of multiples (mtps ≥ 2)
C	1	
C	Kg	grain bulk modulus [Gpa]
C	rnog	grain density [g/cc]
C	Kdry	dry rock bulk modulus [Gpa]
C	uary	dry rock shear modulus [Gpa]
C	pni	porosity normaakilita
C	карра	fluid hulk modulus [Cno]
C	Kl vh o f	fluid density [a/aa]
C	rnoi	fluid density [g/cc]
C	111	fiuld viscosity [cp]
C	Output	
C	Output.	roflactivity sories
C	a b	transmitivity series
C	nsr	number of samples in reflectivity series
C	nst	number of samples in transmitivity series
C		
C C	Input File I	Format:
C	1	
C	nlaver free	u dt mtns
C	kg rhog k	dry udry phi kappa kf rhof pf [Laver 0]
C	kg rhog k	dry, udry, phi, kappa, ki, moi, m [Layer 0] dry, udry, phi, kappa, kf, rhof, nf [Layer 1]
C	kg, mog, k	ury, uury, pin, kappa, ki, mor, m [Layer 1]
C C	kg, rhog, k	dry, udry, phi, kappa, kf, rhof, nf [Layer k]
C	Input File l	Example:
С	1	
Č	3 22	0.0001 3

С	38	2.65	1.46	1.56	0.3	2	0.025	0.15	0.01		
С	38	2.65	1.46	1.56	0.3	2	2.42	1	1		
С	38	2.65	1.46	1.56	0.3	2	0.025	0.15	0.01		
C	NT - 4 - 1	т	0 1 1	· · · · · · · · 1-			- 16				
C	Note:	Layer	r = k + r	∠ayer ĸ	are tw	o n	air space	es.			
C			ц — к + .	1							
C	Refere	References: Silin D., and Goloshubin G. 2008. Seismic									
С		wave reflection from a permeable layer:									
С		low-frequency asymptotic analysis: Proceedings									
С		of IMECE, Boston, USA.									
С		Rol	binson,	E. A., 1	967, 1	Mul	tichanne	el time :	series		
С		an	alysis v	vith dig	ital co	mpi	uter prog	grams:			
C		H	olden-D	Day, Sar	n Fran	cisc	0.				
C			X 7	·····	· \ T	• •	 · T · · ·			2000	
C	Autho	or:	Yang	un (Ke	vin) L	10	Universi	ty of H	ouston	2009	
C	nrogram s	slowave									
	double	e precis	$\frac{1}{100}$	0000) ł	n(1000)())					
	intege	er flag	1011 u (1)	0000), ((1000	,0)					
	intege	i iiug									
	write(*,*) 'Ty	pe 0, to	see sel	lf-doci	ume	nt file'				
	read (*,*) fla	g								
	if(flag	g.eq.0) g	goto 10								
	if(flag.eq.1) goto 20										
10	•. /	* * 1	T1 ·		1 1		а <i>(</i> :	•,	11		
10	write(*,*) \n This program calculates reflectivity and										
	write(*,*) tra		ity seri	es of f	- W2 6 fl	ive and I	BIOL SI	OW mouse'		
	write(*,*) wave propagate through fluid-saturated porous										
	write(*,*) pe		t file is	u med	na. od '					
	write(* *) \n	Input fi	le has f	ormat	cu. bel	ow.'				
	write(* *) '1'	mput n	ite nas i	ormat	UCI	0				
	write(* *) 'nl	aver fre	ea dt n	nultinl	es'					
	write(*.*) 'kg. rhog. kdry. udry. phi. kappa. kf. rhof. nf										
	+ [Laver 0]'										
	write(*,*) 'kg, rhog, kdry, udry, phi. kappa, kf, rhof, nf										
	+ [Layer	1]'	-	-	• •						
	write(*,*) '		'							
	write(*,*) 'kg	, rhog, l	kdry, ud	dry, pł	ni, k	appa, kf	, rhof,	nf		
	+ [Layer]	k]'	_			a	_	_			
	write(*,*) '\n	Examp	le of an	input	file	shows b	below:'			

write(*,*) '1' write(*,*) '3 0.0001 3' 22 write(*,*) '38 2.65 1.46 1.56 0.3 2 0.025 0.15 0.01' +write(*,*) '38 2.65 1.46 1.56 0.3 2 2.42 1 1' +2 write(*,*) '38 2.65 1.46 1.56 0.3 0.025 + $0.15 \quad 0.01 \ n'$ write(*,*) 'This self-document also generates an input file: + input.datn'write(*,*) 'To get output, type: a <input.dat >output.dat\n' write(*,*) 'Check the output in the new file: output.dat\n' open(7,file='input.dat',status='unknown') write(7,*) '1' write(7,*) '3 22 0.0001 3' write(7,*) '38 2.65 1.46 1.56 0.3 2 0.025 + 0.15 0.01' write(7,*) '38 2.65 1.46 1.56 0.3 2 2.42 +1 1' write(7,*) '38 2.65 1.56 0.3 2 0.025 1.46 + $0.15 \quad 0.01 \ n'$ pause goto 100 20 read(*,*) nlayer, freq, dt, mtps write(*,*) \\n nlayer dt[sec] multiples' freq[Hz] write(*,30) nlayer, freq, dt, mtps 30 format(i4,5x,f10.2,8x,f8.6,6x,i4) !/* number of subsurface interfaces */ lc=nlayer-1 call refsl(mtps,lc,freq,dt,a,b,nsr,nst) write(*,*) '\n Reflectivity Slow wave ', nsr call outdat(nsr,a) write(*,*) \\n Transmitivity Slow wave ', nst call outdat(nst,b) 100 stop

end

C											
Ċ		refsl -	calc	ulate r	eflectivit	v and tr	ansmiti	vitv s	eries tak	en	
Ċ			in	ito acco	ount Biot	's slow	wave.				
C											
C		Input:									
Ċ		mtps	nur	mber o	f multipl	es (mtps	s >= 2)				
Ċ		lc	niii	mber o	f subsurf	ace inte	rfaces				
C		frea	fre	aeuncy	[Hz]						
C		dt	sar	nple ra	te or sam	nple time	e [sec]				
C		ut	541	iipie iu	ce or suit	ipie tiin	6 [966]				
C		Output	•								
C		a	ref	lectivit	v series						
$\hat{\mathbf{C}}$		ալյ h[]	tra	nsmitix	vity serie	s					
C		nsr	niii	mber o	f sample	s in refle	ectivity	serie	s		
C		net	nui	mber o	f sample	s in tran	emitivit	ty cor			
C		list	nui		i sampie	5 111 11 411	511111 1 1	.y sci	105		
C-	suł	routine	ref	sl(mtns	s le frea d	lt a h ns	r nst)				
	But	double	nre	cision	$c(4 \ 4) \ c^{2}$	2 cc a(1)	0000 b	(1000	0)		
		double	nre	cision	n1(1000)	n, cc, a(10) (1) $n^2(10)$)000),0()000) a	1(100	(0) $(00) a^{2}(1)$	0000) p(1000))0)
		double	pre	cision	a(1000)	$p_{2(10)}$	(000), q	-2(100	00),q2(1 000)	0000),p(1000	,0)
		double	pre	cision	q(10000)	(10)	(1000), pa	$\frac{1}{2}$	(1000)	pps2(10000)	
		double	pre	cision	pp1(100)	$(0, pp_2)$	(10000)	,pps1	(10000)	,pps2(10000)	
		double	pre	cision	pp(1000) ka(2) rb	(2), qq I(1)	10000),0	$\frac{1}{4}$	(0000)	k_{0}	
		double	pre	cision	kg(2), m kf(2) rhc	f(2) nf(ny(∠),u 2)	ury(2),pm(2),	Kappa(2)	
		double	pre		n11(100)	(2), (10)	(10000)	n12((10000)	14(10000)	
		double	pre		n21(100)	(00), 112(00), 112(00)	(10000) (10000)	, 1113((10000),1	24(10000)	
		double	pre		n21(100)	(00), 1122(00), 1122(00)	(10000)	, 1123((10000),1	124(10000)	
		$\frac{1}{10000},\frac{1}$							134(10000)		
		integer top $1/3$ top - vfeet / velow */					144(10000)				
		integer	tau	. !/ '	r tau = v	last / vsi	low **/				
		oo_1		1/5	k record t	ha agaf	ficiant	outoid	la tha ma	triv */	
		CC=1		!/ " ! /s	^k record			Juisia		urix **/	
		Ise=0		!/*			ber of z	eros		.1v1ty */	
		Isee=0		!/ "		the num	ber of z	eros 1	in transn		
		at_e=0		!/*	* time th	ICKNESS	for top	layer	(nair spa	ice) */	
		maad(*	*) 1	$r_{\alpha}(1)$ m	$rac(1)$ l_{r}	J	d.m. (1) .m	h:(1)	leanna (1	$1_{f}(1)$	
		read(*,	*) K	(g(1),ri	10g(1),KC	iry(1),u	ury(1),)ni(1)	,карра(1),KI(1),	
	+	rnoi(1),ni *) 1	.(1) (2)1	$a = a(2) 1_{a}$	l	d	h :())	lane ()	1-f(2)	
		read(*,	*) K	g(2), r	10g(2), KC	ry(2), u	ury(2),[m(2)	,Kappa(2	2),KI(2),	
	+	rnot(2),nt	(2)	.1	1_ 1			1	1_£	
		write(*	`,*)	n kg	rhog	кdry	udry	phi	карра	KI	
	+	rnof	nr						r 1 - 7		
		write(*	`,*`)	[Gpa]	[g/cc]	[Gpa]	[Gpa]		[darcy]	[Gpa]	

```
+ [g/cc] [cp]'
       write(*,10) kg(1),rhog(1),kdry(1),udry(1),phi(1),kappa(1),kf(1),
       rhof(1), nf(1)
  +
      write(*,10) kg(2),rhog(2),kdry(2),udry(2),phi(2),kappa(2),kf(2),
       rhof(2), nf(2)
  +
10
      format(9f8.3)
      call onelayer(kg,rhog,kdry,udry,phi,kappa,kf,rhof,nf,freq,dt_e,c,c2,
  +
       tau)
      cc=cc*c2
                     !/* ln is the length of polynomials in matrix N k */
      ln=1
                     !/* N_0 = M_0, so \ln = 1 for N_0; N_1 = M_1 * N_0 */
      n11(1)=c(1,1)!
      n12(1)=c(1,2)!
      n13(1)=c(1.3) !!
      n14(1)=c(1,4)!
      n21(1)=c(2,1)!
      n22(1)=c(2,2) !|
      n23(1)=c(2,3)!
      n24(1)=c(2,4) ! > /* form matrix N_0, which equals to M_0 */
      n31(1)=c(3,1)!
      n32(1)=c(3,2)!
      n33(1)=c(3,3)!
      n34(1)=c(3,4)!
      n41(1)=c(4,1) !!
      n42(1)=c(4,2) !|
      n43(1)=c(4,3)!
      n44(1)=c(4,4)!/
      do k=2, lc
                     !/* recursively calculate matrix N_k;
                     ! N_k = M_k * N_{(k-1)} */
        kg(1)=kg(2)
        rhog(1)=rhog(2)
        kdry(1)=kdry(2)
        udry(1)=udry(2)
        phi(1)=phi(2)
        kappa(1)=kappa(2)
        kf(1)=kf(2)
        rhof(1)=rhof(2)
        nf(1)=nf(2)
        read(*,*) kg(2),rhog(2),kdry(2),udry(2),phi(2),kappa(2),kf(2),
```

+	rhof(2),nf(2)
	write(*,10) kg(2),rhog(2),kdry(2),udry(2),phi(2),kappa(2),kf(2),
+	rhof(2),nf(2)

```
rhof(2), nf(2)
```

call onelayer(kg,rhog,kdry,udry,phi,kappa,kf,rhof,nf,freq,dt,c,

```
c2,tau)
+
```

cc=cc*c2	
lse=lse+tau-1	<pre>!/* the zero coefficients in reflectivity ! polynomials increase with tau-1 */</pre>
lsee=lsee+2*tau	<pre>!/* the zero coefficients in transmitivity ! polynomials increase with 2*tau */</pre>
lm=mtps*tau+1	 !/* record the length of polynomials in ! propagator matrix M_k */

```
call mprod(c,tau,lm,ln,n11,n12,n13,n14,n21,n22,n23,n24,n31,n32,
n33,n34,n41,n42,n43,n44)
```

end do

+

```
call fold(ln,n44,ln,n31,lp,p1)
call fold(ln,n41,ln,n34,lp,p2)
call fold(ln,n33,ln,n41,lp,ps1)
call fold(ln,n31,ln,n43,lp,ps2)
```

```
call fold(ln,n13,lp,p1,lpp,pp1)
call fold(ln,n13,lp,p2,lpp,pp2)
call fold(ln,n14,lp,ps1,lpp,pps1)
call fold(ln,n14,lp,ps2,lpp,pps2)
```

```
call fold(ln,n43,ln,n34,lq,q1)
call fold(ln,n44,ln,n33,lq,q2)
call fold(ln,n11,lq,q1,lqq,qq1)
call fold(ln,n11,lq,q2,lqq,qq2)
```

```
do i=1,lpp
```

```
pp(i)=qq1(i)-qq2(i)+pp1(i)-pp2(i)+pps1(i)-pps2(i)
end do
```

call pcut(lpp,pp,lsee) !/* cut the zero coefficients

! in polynomial pp[] */ do i=1,lq q(i)=q1(i)-q2(i)end do !/* cut the zero coefficients call pcut(lq,q,lse) ! in polynomial q[] */ do i=1,lp p(i)=p1(i)-p2(i)end do call pcut(lp,p,lse) !/* cut the zero coefficients ! in polynomial p[] */ С /* reflectivity series, receiver in the top layer (half space) */ call polydv(lq,q,lp,p,lp,a) nsr=lp С /* transmitivity series, receiver in the bottom layer (half space) */ call polydv(lq,q,lpp,pp,lpp,b) do i=1,lpp b(i)=b(i)/cc end do nst=lpp return end C----mprod - carry out matrix multiplication: $N_k = M_k * N_{(k-1)}$ С C-----С Input: matrix N_(k-1) array of coefficients in propagator matrix M С c[] С slow wave time delay factor, tau = vfast / vslow tau С lm length of polynomials in propagator matrix M k С length of polynomials in matrix N_(k-1) ln С n11 - n44 polynomials in matrix N_(k-1)

С С matrix N_k Output: С length of polynomials in matrix N_k ln С n11 - n44 polynomials of the matrix elements in matrix N k C-_____ С Note: multiplication of polynomials is essentially a С convolution of their coefficients C----_____ subroutine mprod(c,tau,lm,ln,n11,n12,n13,n14,n21,n22,n23, + n24,n31,n32,n33,n34,n41,n42,n43,n44) integer tau double precision c(4,4)double precision n11(10000),n12(10000),n13(10000),n14(10000) double precision n21(10000),n22(10000),n23(10000),n24(10000) double precision n31(10000),n32(10000),n33(10000),n34(10000) double precision n41(10000),n42(10000),n43(10000),n44(10000) double precision m11(10000),m12(10000),m13(10000),m14(10000) double precision m21(10000),m22(10000),m23(10000),m24(10000) double precision m31(10000),m32(10000),m33(10000),m34(10000) double precision m41(10000),m42(10000),m43(10000),m44(10000) double precision n11a(10000),n12a(10000),n13a(10000),n14a(10000) double precision n21a(10000),n22a(10000),n23a(10000),n24a(10000) double precision n31a(10000),n32a(10000),n33a(10000),n34a(10000) double precision n41a(10000),n42a(10000),n43a(10000),n44a(10000) double precision n11b(10000),n12b(10000),n13b(10000),n14b(10000) double precision n21b(10000),n22b(10000),n23b(10000),n24b(10000) double precision n31b(10000),n32b(10000),n33b(10000),n34b(10000) double precision n41b(10000),n42b(10000),n43b(10000),n44b(10000) double precision n11c(10000),n12c(10000),n13c(10000),n14c(10000) double precision n21c(10000),n22c(10000),n23c(10000),n24c(10000) double precision n31c(10000),n32c(10000),n33c(10000),n34c(10000) double precision n41c(10000),n42c(10000),n43c(10000),n44c(10000) double precision n11d(10000),n12d(10000),n13d(10000),n14d(10000) double precision n21d(10000),n22d(10000),n23d(10000),n24d(10000) double precision n31d(10000),n32d(10000),n33d(10000),n34d(10000) double precision n41d(10000),n42d(10000),n43d(10000),n44d(10000)

call zero(lm,m11) !\ m11(tau+2)=c(1,1) !| call zero(lm,m12) !| m12(2*tau+1)=c(1,2) !| call zero(lm,m13) !| m13(tau)=c(1,3)!| call zero(lm,m14) !| m14(1)=c(1,4)!| call zero(lm,m21) !| m21(tau+2)=c(2,1)!| call zero(lm,m22) !| m22(2*tau+1)=c(2,2)!!| call zero(lm,m23) !| m23(tau)=c(2,3)call zero(lm,m24) !| ! > /* form propagator matrix M k */ m24(1)=c(2,4)call zero(lm,m31) !| m31(tau+2)=c(3,1)!| call zero(lm,m32) !| m32(2*tau+1)=c(3,2)!call zero(lm,m33) !| !| m33(tau)=c(3,3)call zero(lm,m34) !| m34(1)=c(3,4)!| !| call zero(lm,m41) !| m41(tau+2)=c(4,1)call zero(lm,m42) !| m42(2*tau+1)=c(4,2)!call zero(lm,m43) !| m43(tau)=c(4,3)!| call zero(lm,m44) !| m44(1)=c(4,4)!/ call fold(lm,m11,ln,n11,j,n11a) call fold(lm,m12,ln,n21,j,n11b)

call fold(lm,m12,ln,n21,j,n11b) call fold(lm,m13,ln,n31,j,n11c) call fold(lm,m14,ln,n41,j,n11d) call fold(lm,m11,ln,n12,j,n12a) call fold(lm,m12,ln,n22,j,n12b) call fold(lm,m13,ln,n32,j,n12c) call fold(lm,m14,ln,n42,j,n12d) call fold(lm,m11,ln,n13,j,n13a) call fold(lm,m12,ln,n23,j,n13c) call fold(lm,m14,ln,n43,j,n13d) call fold(lm,m11,ln,n14,j,n14a) call fold(lm,m12,ln,n24,j,n14b) call fold(lm,m13,ln,n34,j,n14c) call fold(lm,m14,ln,n44,j,n14d)

call fold(lm,m21,ln,n11,j,n21a) call fold(lm,m22,ln,n21,j,n21b) call fold(lm,m23,ln,n31,j,n21c) call fold(lm,m24,ln,n41,j,n21d) call fold(lm,m21,ln,n12,j,n22a) call fold(lm,m22,ln,n22,j,n22b) call fold(lm,m23,ln,n32,j,n22c) call fold(lm,m24,ln,n42,j,n22d) call fold(lm,m21,ln,n13,j,n23a) call fold(lm,m22,ln,n23,j,n23b) call fold(lm,m23,ln,n33,j,n23c) call fold(lm,m24,ln,n43,j,n23d) call fold(lm,m21,ln,n14,j,n24a) call fold(lm,m22,ln,n24,j,n24b) call fold(lm,m23,ln,n34,j,n24c) call fold(lm,m24,ln,n44,j,n24d)

call fold(lm,m31,ln,n11,j,n31a) call fold(lm,m32,ln,n21,j,n31b) call fold(lm,m33,ln,n31,j,n31c) call fold(lm,m34,ln,n41,j,n31d) call fold(lm,m31,ln,n12,j,n32a) call fold(lm,m32,ln,n22,j,n32b) call fold(lm,m33,ln,n32,j,n32c) call fold(lm,m34,ln,n42,j,n32d) call fold(lm,m31,ln,n13,j,n33a) call fold(lm,m32,ln,n23,j,n33b) call fold(lm,m33,ln,n33,j,n33c) call fold(lm,m34,ln,n43,j,n33d) call fold(lm,m31,ln,n14,j,n34a) call fold(lm,m32,ln,n24,j,n34b) call fold(lm,m33,ln,n34,j,n34c) call fold(lm,m34,ln,n44,j,n34d)

call fold(lm,m41,ln,n11,j,n41a) call fold(lm,m42,ln,n21,j,n41b) call fold(lm,m43,ln,n31,j,n41c) call fold(lm,m44,ln,n41,j,n41d) call fold(lm,m41,ln,n12,j,n42a) call fold(lm,m42,ln,n22,j,n42b) call fold(lm,m43,ln,n32,j,n42c)

```
call fold(lm,m41,ln,n13,j,n43a)
call fold(lm,m42,ln,n23,j,n43b)
call fold(lm,m43,ln,n33,j,n43c)
call fold(lm,m44,ln,n43,j,n43d)
call fold(lm,m41,ln,n14,j,n44a)
call fold(lm,m42,ln,n24,j,n44b)
call fold(lm,m43,ln,n34,j,n44c)
call fold(lm,m44,ln,n44,j,n44d)
do k=1,j
 n11(k)=n11a(k)+n11b(k)+n11c(k)+n11d(k)
end do
do k=1,j
 n12(k)=n12a(k)+n12b(k)+n12c(k)+n12d(k)
end do
do k=1,j
 n13(k)=n13a(k)+n13b(k)+n13c(k)+n13d(k)
end do
do k=1,j
 n14(k)=n14a(k)+n14b(k)+n14c(k)+n14d(k)
end do
do k=1,i
 n21(k)=n21a(k)+n21b(k)+n21c(k)+n21d(k)
end do
do k=1,j
 n22(k)=n22a(k)+n22b(k)+n22c(k)+n22d(k)
end do
do k=1,j
 n23(k)=n23a(k)+n23b(k)+n23c(k)+n23d(k)
end do
do k=1,j
 n24(k)=n24a(k)+n24b(k)+n24c(k)+n24d(k)
end do
do k=1,j
 n31(k)=n31a(k)+n31b(k)+n31c(k)+n31d(k)
end do
do k=1,j
 n32(k)=n32a(k)+n32b(k)+n32c(k)+n32d(k)
end do
do k=1,i
 n33(k)=n33a(k)+n33b(k)+n33c(k)+n33d(k)
end do
```

call fold(lm,m44,ln,n42,j,n42d)

```
do k=1,j
      n34(k)=n34a(k)+n34b(k)+n34c(k)+n34d(k)
     end do
     do k=1,j
      n41(k)=n41a(k)+n41b(k)+n41c(k)+n41d(k)
     end do
     do k=1,j
      n42(k)=n42a(k)+n42b(k)+n42c(k)+n42d(k)
     end do
     do k=1,j
      n43(k)=n43a(k)+n43b(k)+n43c(k)+n43d(k)
     end do
     do k=1,j
      n44(k)=n44a(k)+n44b(k)+n44c(k)+n44d(k)
     end do
          !/* update the length of polynomials in matrix N_k */
     ln=j
  return
  end
C-----
     outdat - print out the values of array x[lx]
С
C-----
  subroutine outdat(lx,x)
     double precision x(lx)
     write(^{*},5) (x(i),i=1,lx)
5
     format(f30.16)
  return
  end
C-----
     pcut - cut the beginning k values of array P[lp]
С
C-----
  subroutine pcut(lp,p,k)
     double precision p(lp)
     lp=lp-k
     do i=1,lp
      p(i)=p(i+k)
     end do
  return
  end
```

```
C-----
       _____
С
     polydv - polynomials division (Robinson, 1967)
C-----
С
     Input:
С
          length of dvs[]
     n
С
     dvs[] array of polynomial coefficients
С
          length of dvd[]
     m
С
     dvd[] array of polynomial coefficients
С
С
     Output:
С
     1
          length of q[]
С
          array of polynomial coefficients: q[] = dvd[] / dvs[]
     q[]
C---
        -----
С
     Note: q[1] must not equal to 0
C-----
  subroutine polydv(n,dvs,m,dvd,l,q)
     double precision dvs(n),dvd(m),q(l)
     call zero (l,q)
     call move(min(m,l),dvd,q)
     do i=1,1
      q(i)=q(i)/dvs(1)
      if(i.eq.l) return
      k=i
      isub=min(n-1,l-i)
      do j=1,isub
       k=k+1
       q(k)=q(k)-q(i)*dvs(j+1)
      end do
     end do
  return
  end
C-----
С
     fold - polynomial multiplication (Robinson, 1967)
C-----
С
     Input:
С
          length of a[]
     la
С
     a[]
          array of polynomial coefficients
          length of b[]
С
     lb
С
     b[]
          array of polynomial coefficients
С
С
     Output:
С
          length of c[]
     lc
```

```
С
     c[]
         array of polynomial coefficients:
C-----
С
    Note: c[] is essentially the convolution of a[] and b[]
С-----
  subroutine fold(la,a,lb,b,lc,c)
    double precision a(la),b(lb),c(lc)
    lc=la+lb-1
    call zero(lc,c)
    do i=1,la
     do j=1,lb
      k=i+j-1
      c(k)=c(k)+a(i)*b(j)
     end do
    end do
  return
  end
C-----
С
    move - copy the values of array x to array y (Robinson, 1967)
C-----
С
    Input:
С
         length of x[] and y[]
     lx
С
         array of polynomial coefficients
     x[]
С
С
    Output:
С
     y[]
         array of polynomial coefficients
C-----
  subroutine move(lx,x,y)
    double precision x(lx), y(lx)
    do i=1,lx
     y(i)=x(i)
    end do
  return
  end
C-----
С
    zero - form zero array (Robinson, 1967)
C-----
С
    Input:
С
    lx
         length of x[]
С
         array of polynomial coefficients
     x[]
С
С
    Output:
```

C C	x[] array of all zero values
c	subroutine zero(lx,x) double precision x(lx) if ($lx.le.0$) return do i=1, lx x(i)=0.0 end do return end
C- C C C	onelayer - calculates reflections using asymptotic formulas of Biot for one layer of medium (reference: Silin & Goloshubin, 2008).
	Input: kg grain bulk modulus rhog grain density kdry dry rock bulk modulus udry dry rock shear modulus phi porosity kappa permeability kf fluid bulk modulus rhof fluid density nf fluid viscosity freq frequency dt sample rate or P wave time thickness of medium [1] Output: c1[] array of coefficients in propagator matrix M c2 coefficients outside the propagator matrix M tau slow wave time delay factor, tau = vfast / vslow
C- C C C-	Note: Wave propagates from medium [1] to medium [2] as down going, from [2] to [1] as up going.
_ -	<pre>subroutine onelayer(kg,rhog,kdry,udry,phi,kappa,kf,rhof,nf, + freq,dt,c1,c2,tau) double precision kg(2),rhog(2),kdry(2),udry(2),phi(2),kappa(2) double precision kf(2),rhof(2),nf(2) double precision ksg_1,ksg_2,ksg_1up,ksg_2up,kfg_1,kfg_2 double precision kfg_1up,kfg_2up</pre>

double precision ks_1,ks_2,ks_1up,ks_2up,m_1,m_2,m_1up,m_2up double precision c1(4,4),c2 integer tau

C Input parameters

pi=3.141592654 w=2*pi*freq

C Calculation for down going wave

```
m_1 = kdry(1) + udry(1) * 4/3
   m_2 = kdry(2) + udry(2) * 4/3
   bf 1=1/kf(1)
   bf 2=1/kf(2)
   rhobulk 1=phi(1)*rhof(1)+(1-phi(1))*rhog(1)
   rhobulk_2=phi(2)*rhof(2)+(1-phi(2))*rhog(2)
   gk=rhof(2)*nf(1)*kappa(2)/(rhof(1)*nf(2)*kappa(1))
   gro 1=rhobulk 1/rhof(1)
   gro_2=rhobulk_2/rhof(2)
   e=0.000000986923*rhof(2)*kappa(2)*w/nf(2)
   vb_1=1000*sqrt(m_1/rhobulk_1)
   vb_2=1000*sqrt(m_2/rhobulk_2)
   vf 1=1000*sqrt(m 1/rhof(1))
   vf 2=1000*sqrt(m 2/rhof(2))
   ksg_1=kg(1)/(1-phi(1))
   ksg 2=kg(2)/(1-phi(2))
   kfg_1=kg(1)/(1-kdry(1)/kg(1))
   kfg 2=kg(2)/(1-kdry(2)/kg(2))
   gb_1=m_1*(bf_1*phi(1)+(1-phi(1))/kfg_1)
   gb_2=m_2*(bf_2*phi(2)+(1-phi(2))/kfg_2)
   gm_1=1-(1-phi(1))*kdry(1)/ksg_1
   gm_2=1-(1-phi(2))*kdry(2)/ksg_2
   z_1=10**6*m_1*sqrt((gb_1+gm_1**2)/gb_1)/vb_1
   z_2=10**6*m_2*sqrt((gb_2+gm_2**2)/gb_2)/vb_2
   a = (gm_1/(gm_1**2+gb_1)-gm_2/(gm_2**2+gb_2))*2*z_1*z_2/(z_1+z_2)
   d=0.000001*z 1*z 2*sqrt(gb 1*gb 2)*(vb 1*sqrt(gm 1**2+gb 1)/
$
    (sqrt(gk)*gro_2*m_1)+vb_2*sqrt(gm_2**2+gb_2)/(gro_1*m_2))/
$
   (gm_1*gm_2)
```

C Calculation for up going wave

 $m_1up=kdry(2)+udry(2)*4/3$

```
m_2up=kdry(1)+udry(1)*4/3
   bf_1up=1/kf(2)
   bf_2up=1/kf(1)
   rhobulk_1up=phi(2)*rhof(2)+(1-phi(2))*rhog(2)
   rhobulk_2up=phi(1)*rhof(1)+(1-phi(1))*rhog(1)
   gkup=rhof(1)*nf(2)*kappa(1)/(rhof(2)*nf(1)*kappa(2))
   gro_1up=rhobulk_1up/rhof(2)
   gro_2up=rhobulk_2up/rhof(1)
   eup=0.000000986923*rhof(1)*kappa(1)*w/nf(1)
   vb_1up=1000*sqrt(m_1up/rhobulk_1up)
   vb 2up=1000*sqrt(m 2up/rhobulk 2up)
   vf 1up=1000*sqrt(m 1up/rhof(2))
   vf_2up=1000*sqrt(m_2up/rhof(1))
   ksg_1up=kg(2)/(1-phi(2))
   ksg 2up=kg(1)/(1-phi(1))
   kfg 1up=kg(2)/(1-kdry(2)/kg(2))
   kfg_2up=kg(1)/(1-kdry(1)/kg(1))
   gb_1up=m_1up*(bf_1up*phi(2)+(1-phi(2))/kfg_1up)
   gb 2up=m 2up*(bf 2up*phi(1)+(1-phi(1))/kfg 2up)
   gm_1up=1-(1-phi(2))*kdry(2)/ksg_1up
   gm 2up=1-(1-phi(1))*kdry(1)/ksg 2up
   z_1up=10**6*m_1up*sqrt((gb_1up+gm_1up**2)/gb_1up)/vb_1up
   z_2up=10**6*m_2up*sqrt((gb_2up+gm_2up**2)/gb_2up)/vb_2up
   aup=(gm_1up/(gm_1up**2+gb_1up)-gm_2up/(gm_2up**2+gb_2up))*
2*z \ 1up*z \ 2up/(z \ 1up+z \ 2up)
   dup=0.000001*z_1up*z_2up*sqrt(gb_1up*gb_2up)*
   (vb lup*sqrt(gm lup**2+gb lup)/(sqrt(gkup)*gro 2up*m lup)+
   vb_2up*sqrt(gm_2up**2+gb_2up)/(gro_1up*m_2up))/(gm_1up*gm_2up)
   Reflection coefficients and transmission coefficients
   For fast incident and down going wave
```

 $r_1fs = (gm_2 * *2 + gb_2) * a/(gm_2 * d)$ $t_1fs = (gm_1 * * 2 + gb_1) * a/(gm_1 * d)$ $r_1ff=z_2*(t_1fs-r_1fs)/(z_1+z_2)$ $t_1ff=z_1*(r_1fs-t_1fs)/(z_1+z_2)$ $rff=(z_1-z_2)/(z_1+z_2)+sqrt(e)*r_1ff/2**0.5$ rffi=sqrt(e)*r 1ff/2**0.5 $tff=1+(z_1-z_2)/(z_1+z_2)+sqrt(e)*t_1ff/2**0.5$ tffi=sqrt(e)*t 1ff/2**0.5 rfs=r 1fs*sqrt(e)/2**0.5 rfsi=r 1fs*sqrt(e)/2**0.5

\$

\$

С

С

tfs=t_1fs*sqrt(e)/2**0.5 tfsi=t_1fs*sqrt(e)/2**0.5

C For fast incident and up going wave

 $r_1fsup=(gm_2up^{**}2+gb_2up)^{*}aup/(gm_2up^{*}dup)$ $t_1fsup=(gm_1up^{**}2+gb_1up)^{*}aup/(gm_1up^{*}dup)$ $r_1ffup=z_2up^{*}(t_1fsup-r_1fsup)/(z_1up+z_2up)$ $t_1ffup=z_1up^{*}(r_1fsup-t_1fsup)/(z_1up+z_2up)$ $rffup=(z_1up-z_2up)/(z_1up+z_2up)+sqrt(eup)^{*}r_1ffup/2^{**}0.5$ $rffiup=sqrt(eup)^{*}r_1ffup/2^{**}0.5$ $tffup=1+(z_1up-z_2up)/(z_1up+z_2up)+sqrt(eup)^{*}t_1ffup/2^{**}0.5$ $rfsup=r_1fsup^{*}sqrt(eup)/2^{**}0.5$ $rfsup=r_1fsup^{*}sqrt(eup)/2^{**}0.5$ $tfsup=t_1fsup^{*}sqrt(eup)/2^{**}0.5$ $tfsup=t_1fsup^{*}sqrt(eup)/2^{**}0.5$ $tfsup=t_1fsup^{*}sqrt(eup)/2^{**}0.5$

C For slow incident and down going wave

```
cs_1=gm_1+gb_1/gm_1
cs_2=gm_2+gb_2/gm_2
xs_1=-1/gm_1
xs_2=-1/gm_2
ks_1=(1/vf_1)*sqrt(gb_1+gm_1**2)
ks_2=(1/vf_2)*sqrt(gb_2+gm_2**2)
rss=(-cs_1*m_2*ks_2*xs_2/sqrt(gk)+cs_2*m_1*ks_1*xs_1)/
```

- $\begin{array}{l} & (cs_1*m_2*ks_2*xs_2/sqrt(gk)+cs_2*m_1*ks_1*xs_1) \\ & tss=\!(cs_2*m_2*ks_2*xs_2/sqrt(gk)+cs_1*m_1*ks_1*xs_1)/ \end{array}$
- $\begin{array}{l} & (cs_1*m_2*ks_2*xs_2/sqrt(gk)+cs_2*m_1*ks_1*xs_1) \\ & rsf=z_2*(-1-rss+tss)/(z_1+z_2) \\ & tsf=-z_1*(-1-rss+tss)/(z_1+z_2) \end{array}$
- C For slow incident and up going wave

```
cs_lup=gm_lup+gb_lup/gm_lup

cs_2up=gm_2up+gb_2up/gm_2up

xs_lup=-1/gm_lup

xs_2up=-1/gm_2up

ks_lup=(1/vf_lup)*sqrt(gb_lup+gm_lup**2)

ks_2up=(1/vf_2up)*sqrt(gb_2up+gm_2up**2)

rssup=(-cs_lup*m_2up*ks_2up*xs_2up/sqrt(gkup)+
```

 $cs_2up*m_1up*ks_1up*xs_1up)/(cs_1up*m_2up*ks_2up*$

- \$ xs_2up/sqrt(gkup)+cs_2up*m_1up*ks_1up*xs_1up)
 tssup=(cs_2up*m_2up*ks_2up*xs_2up/sqrt(gkup)+cs_1up*
- \$ m_1up*ks_1up*xs_1up)/(cs_1up*m_2up*ks_2up*xs_2up/
- \$ sqrt(gkup)+cs_2up*m_1up*ks_1up*xs_1up)
 rsfup=z_2up*(-1-rssup+tssup)/(z_1up+z_2up)
 tsfup=-z_1up*(-1-rssup+tssup)/(z_1up+z_2up)
- C Velocity and attenuation coefficient

```
vfast_1=vb_1*sqrt(1+gm_1**2/gb_1)

vfast_2=vb_2*sqrt(1+gm_2**2/gb_2)

vslow_1=vf_1*sqrt(2*eup/(gb_1+gm_1**2))

vslow_2=vf_2*sqrt(2*e/(gb_2+gm_2**2))

zeta_0_1=(gm_1**2+gb_1)/(gb_1*gro_1)

zeta_0_2=(gm_2**2+gb_2)/(gb_2*gro_2)

zeta_1_1=(((gm_1**2+gb_1)/gro_1)-gm_1)**2/(gb_1*(gm_1**2+gb_1)))

zeta_1_2=(((gm_2**2+gb_2)/gro_2)-gm_2)**2/(gb_2*(gm_2**2+gb_2)))

afast_1=w*sqrt(gb_1/(gb_1+gm_1**2))*zeta_1_1*eup/(vb_1*2*zeta_0_1))

afast_2=w*sqrt(gb_2/(gb_2+gm_2**2))*zeta_1_2*e/(vb_2*2*zeta_0_2)

aslow_1=w*sqrt((gb_1+gm_1**2)/(2*eup))/vf_1

aslow_2=w*sqrt((gb_2+gm_2**2)/(2*e))/vf_2
```

C For purely elastic media

 $rff_elastic=(z_1-z_2)/(z_1+z_2)$ $tff_elastic=1+(z_1-z_2)/(z_1+z_2)$ $rffup_elastic=(z_1up-z_2up)/(z_1up+z_2up)$ $tffup_elastic=1+(z_1up-z_2up)/(z_1up+z_2up)$

C Calculate the Matrix elements of M_0

att_f=exp(-afast_1*vfast_1*dt)
att_s=exp(-aslow_1*vfast_1*dt)

c1(1,1)=(tff*(tffup*tssup-tsfup*tfsup)+rffup*

- $(-tssup*rff+tsfup*rfs)+rsfup*(-rfs*tffup+rff*tfsup))*att_f c1(1,2)=(tsf*(tffup*tssup-tsfup*tfsup)+rffup*$
- \$ (-tssup*rsf+tsfup*rss)+rsfup*(-rss*tffup+rsf*tfsup))*att_s
 c1(1,3)=(rffup*tssup-rsfup*tfsup)/att_f
 c1(1,4)=(-rffup*tsfup+rsfup*tffup)/att_s
 c1(2,1)=(tfs*(tffup*tssup-tsfup*tfsup)+rfsup*
- \$ (-tssup*rff+tsfup*rfs)+rssup*(-rfs*tffup+rff*tfsup))*att_f
 c1(2,2)=(tss*(tffup*tssup-tsfup*tfsup)+rfsup*

tau=vfast_1/vslow_1

return end